ShakeMap & Related Products: Challenges in Real-time Shaking & Loss Estimation

David Wald (for B. Worden, K. Lin, G. Hayes,...)

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Workshop on National Geophysical Networks in Latin America Universidad de Chile, Santiago, Chile May 25-29, 2015











Global variations of "unsafe" buildings



Figure 1.1 Graph summarising responses from international earthquake engineers on percentage of seismically unsafe buildings in their country (Spence, 2007b).

ShakeCast

PAGER (Prompt Assessment of Global Earthquakes for Response)



ShakeCast

PAGER (Prompt Assessment of Global Earthquakes for Response)





"Did You Feel It?"

ShakeMap



"Did You Feel It?"

ShakeMap

USGS Community Internet Intensity Map NORTHERN CALIFORNIA Aug 24 2014 03:20:44 AM local 38.2202N 122.3128W M6.0 Depth: 11 km ID:nc72282711 Magnitude 6.0 2014 South Napa, CA Elk Gro **Felt Report** Your location when the earthquake occurred Choose Location Did you feel it? Yes No The remainder of this form is optional. Help make a shaking intensity map by telling us about the shaking at your location. What was your situation during the earthquake? Not specified Inside a building Outside a building In a stopped vehicle In a moving vehicle Other Were you asleep? Submit Cance

CISN Peak Velocity Map (in cm/s) : 6.4 km (4.0 mi) NW of American Canyon, CA Aug 24, 2014 10:20:44 AM UTC M 6.0 N38.22 W122.31 Depth: 11.7km ID:72282711



Map Version 28 Processed 2014-08-29 12:45:01 PM PDT

PERCEIVED SHAKING	Not felt	Weak	Light	Moderate	Strong	Very strong	Severe	Violent	Extreme
POTENTIAL DAMAGE	none	none	none	Very light	Light	Moderate	Mod./Heavy	Heavy	Very Heavy
PEAK ACC.(%g)	<0.1	0.5	2.4	6.7	13	24	44	83	>156
PEAK VEL.(cm/s)	<0.07	0.4	1.9	5.8	11	22	43	83	>160
INSTRUMENTAL INTENSITY	I	-	IV	V	VI	VII	VIII	IX	Х+

Scale based upon Wald, et al.; 1999





Scale based upon Wald, et al.; 1999





Scale based upon W	orden et al.	2012)			1				
INSTRUMENTAL INTENSITY	- 1	11-111	IV	V	VI	VII	VIII	IX	X+
PEAK VEL.(cm/s)	<0.02	0.1	1.4	4.7	9.6	20	41	86	>178
PEAK ACC.(%g)	<0.05	0.3	2.8	6.2	12	22	40	75	>139
DAMAGE	none	none	none	Very light	Light	Moderate	Mod./Heavy	Heavy	Very Heavy
SHAKING	Not telt	weak	Light	Moderate	Strong	very strong	Severe	violent	Extreme

6 min ShakeMap 15 min

6 hrs



	Google Earth
La Intensity L II-III IV V VI VII VIII II LO Shaking Not felt Weak Light Moderate Strong Very Strong Severe Violent Extreme Damage None None Very Light Light Moderate Moderate/ Heavy Very Heavy	ke Winnipeg Canadian Shield
Rocky Mountains	Lake Superfor Clake Superfor Overgehan Bay
Magnitude 6.0 2014 South Napa, CA	Lake Mitchigan.
	ted States
	Mineral, VA
Data rate 4328 kbps (Net: total 720 kB qps 2.23, rate 121 kbps, Disk: total 24 Rock latency averages = net 70.00 ms o	net 5.87%) - total size 25707 kB avg latency 38.34 ms, min 15.21 ms, max 108.92 ms 1987 kB rate 4207 kbps lisk 0.00 ms deserialize 0.00 ms overall 70.00 ms









Processed: Wed Aug 24 11:12:25 2011

PERCEIVED SHAKING	Not felt	Weak	Light	Moderate	Strong	Very strong	Severe	Violent	Extreme
POTENTIAL DAMAGE	none	none	none	Very light	Light	Moderate	Moderate/Heavy	Heavy	Very Heavy
PEAK ACC.(%g)	<.17	.17-1.4	1.4-3.9	3.9-9.2	<i>9.2</i> -18	18-34	34-65	65-124	>124
PEAK VEL.(cm/s)	<0.1	0.1-1.1	1.1-3.4	3.4-8.1	8.1-16	16-31	31-60	60-116	>116
INSTRUMENTAL INTENSITY	I	-	IV	V	VI	VII	VIII	IX	X+





"Did You Feel It?"

ShakeMap





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INSTRUMENTAL INTENSITY	I	11-111	IV	V	VI	VII	VIII	IX	X+







Vs30 Site amplification map from topographic slope

(Wald & Allen, 2007)

Map Version 6 Processed Sat Sep 8, 2012 02:12:28 PM MDT

PEAK VEL.(cm/s)	<0.02	0.1	1.4	4.7	9.6	20	41	86	>178
INSTRUMENTAL INTENSITY	I	-	IV	V	VI	VII	VIII	IX	X+

Scale based upon Worden et al. (2011)



Final map of California resulting from kriging with a trend on the hybrid Wills and Calahan (2006) Vs30 map.

[Thompson, Worden & Wald, 2014]

SEP 5 2012 02:42:08 PM GMT M 7.6 N10.09 W85.31 Depth: 40.0km ID:c000cfsd Bluefi 12° Quesad 10° 8° km 100 0 –84° -88° –86° Map Version 6 Processed Sat Sep 8, 2012 02:12:28 PM MDT PEAK VEL.(cm/s) <0.02 4.7 9.6 20 41 0.1 1.4 INSTRUMENTAL IV V VI 11-111 VII VIII INTENSITY

USGS ShakeMap : COSTA RICA

Scale based upon Worden et al. (2011)



Intensity in California

by C. B. Worden, M. C. Gerstenberger, D. A. Rhoades, and D. J. Wald

Bull. Seism. Soc. Am. (2010)

Abstract We use a database of approximately 200,000 modified Mercalli intensity (MMI) observations of California earthquakes collected from USGS "Did You Feel It?" (DYFI) reports, along with a comparable number of peak ground-motion amplitudes from California seismic networks, to develop probabilistic relationships between MMI and peak ground velocity (PGV), peak ground acceleration (PGA), and 0.3 s, 1 s, and 3 s 5% damped pseudospectral acceleration (PSA). After associating each groundmotion observation with an MMI computed from all the DYFI responses within 2 km of the observation, we derived a joint probability distribution between MMI and ground motion. We then derived reversible relationships between MMI and each ground-motion parameter by using a total least squares regression to fit a bilinear function to the median of the stacked probability distributions. Among the relationships, the fit to peak ground velocity has the smallest errors, though linear combinations of PGA and PGV give nominally better results. We also find that magnitude and distance terms reduce the overall residuals and are justifiable on an information theoretic basis. For intensities MMI ≥ 5, our results are in close agreement with the relations of Wald, Quitoriano, Heaton, Kanamori (1999); for lower intensities, our results fall midway between Wald, Quitoriano, Heaton, Kanamori (1999) and those of Atkinson and Kaka (2007). The earthquakes in the study ranged in magnitude from 3.0 to 7.3, and the distances ranged from less than a kilometer to about 400 km from the source.

Hypocenter & **Magnitude only**

+ DYFI? Data & Fault

+ Strong Motion Stations from Univ. CR

USGS ShakeMap : COSTA RICA USGS ShakeMap : COSTA RICA USGS ShakeMap : COSTA RICA :10 PM GMT M 7.6 N10.12 W85.35 Depth: 40.8km ID:c000c)2:42:08 PM GMT M 7.6 N10.09 W85.31 Depth: 40.0km ID:c000cfsd



INSTRUMENTAL INTENSITY	1	11–111	IV	V	VI	VII	VIII	IX	Х
PEAK VEL.(cm/s)	<0.02	0.1	1.4	4.7	9.6	20	41	86	>1
PEAK ACC.(%g)	<0.05	0.3	2.8	6.2	12	22	40	75	>1
POTENTIAL DAMAGE	none	none	none	Very light	Light	Moderate	Mod./Heavy	Heavy	Very H
SHAKING	Not felt	Weak	Light	Moderate	Strong	Very strong	Severe	Violent	Extre

ale based upon Worden et al. (2011)

Hypocenter

DYFI? + Finite Fault

+ Stations from UCR



GROUND MOTION UNCERTAINTY

ShakeMap grid.xml file

<shakemap_grid xsi:schemaLocation="http://earthquake.usgs.gov/http://earthquake.usgs.gov/eqcenter/shakemap/xml/schemas/shakemap.xsd" event_id="Northridge" shakemap_id="Northridge" shakemap_version="12" code_version="3.2" process_timestamp="2007-01-30T16:07:03Z" shakemap_originator="ci" map_status="RELEASED" shakemap_event_type="ACTUAL"> <event magnitude="6.7" depth="18" lat="34.213000" lon="-118.535700" event_timestamp="1994-01-17T12:30:55GMT" event_description="Northridge"/> <grid_specification lon_min="-119.785700" lat_min="33.379666" lon_max="-117.285700" lat_max="35.046333" nominal_lon_spacing="0.016667" nominal_lat_spacing="0.016667"</pre> nlon="151" nlat="101" nominal pga std="0.520000"/> <grid_field index="1" name="LON" units="dd"/> <grid_field index="2" name="LAT" units="dd"/> <grid_field index="3" name="PGA" units="pctg"/> Grid uncertainty value, Vs30 <grid_field index="4" name="PGV" units="cms"/> <grid_field index="5" name="MMI" units="mmi"/> <grid_field index="6" name="PSA03" units="pctg"/> <grid_field index="7" name="PSA10" units="pctg"/> <grid field index="8" name="PSA30" units="pctg"/> <grid_field index="9" name="SDPGA" units="pctg"/> <grid_field index="10" name="SVEL" units="ms"/> 5.046333 6.3811 4.3655 4.9500 10.9535 5.2248 1.0340 1.0000 372.0000 Lon Lat PGA PGV MMI SA.3 SA1 SA3 Sig. Vs30 0 6333 6.4854 4.4404 4.9600 11.1607 5.3151 1.0521 1.0000 372.0000 -119,719033 35,046333 6,0571 3,8717 4,9000 10,4353 4,6342 0,9174 1,0000 464,0000 -119,70236 6333 6.0963 3.8962 4.9000 10.5136 4.6631 0.9231 1.0000 464.0000 -119.685700 35.046333 6.1375 3.9222 4.9100 10.5959 4.6938 0.9293 1.0000 464.0000 -119.669033 35.046333 6.1914 3.9585 4.9200 10.7029 4.7376 0.9381 1.0000 464.0000 -119.652367 35.046333 6.2471 3.9962 4.9200 10.8134 4.7831 0.9472 1.0000 464.0000 -119.635700 35.046333 6.2991 4.0307 4.9300 10.9167 4.8246 0.9556 1.0000 464.0000 -119.619033 35.046333 7.3392 5.3832 5.1200 12.7334 6.4431 1.2763 1.0000 301.0000 -119.602367 35.046333 7.3890 5.4191 5.1300 12.8329 6.4855 1.2848 1.0000 301.0000 -119.585700 35.046333 7.4410 5.4570 5.1400 12.9372 6.5303 1.2938 1.0000 301.0000 -119.569033 35.046333 6.4927 4.152 4.9000 11.3035 4.9740 0.9857 1.0000 464.0000 -119.552367 35.046333 6.5532 4.1971 4.9700 11 4242 5 0222 0 0056 1 0000 464 0000 $\frac{1}{0000}$ 464.0000 -119.519033 35.046333 7.7020 5.6563 5.180 .0000 301.0000 Ground motion estimates -119.485700 35.046333 7.2820 4.9974 5.110 .0000 372.0000 -119.452367 35.046333 7.4205 5.0975 5.130 .0000 464.0000 -119.419033 35.046333 8.0902 5.9490 5.250 .0000 372.0000 -119.385700 35.046333 8.2042 6.0323 5.270 Intensity (MMI) .0000 301.0000 -119.352367 35.046333 8.3626 6.1547 5.300 .0000 301.0000 -119.319033 35.046333 8.5002 6.2587 5.320 .0000 301.0000 • Peak ground acceleration (PGA) -119.285700 35.046333 8.6174 6.3445 5.340 .0000 301.0000 -119.252367 35.046333 8.7839 6.4734 5.360 .0000 301.0000 -119.219033 35.046333 8.9254 6.5806 5.390 • Peak ground velocity (PGV) .0000 301.0000 -119.185700 35.046333 9.0423 6.6664 5.400 .0000 301.0000 -119.152367 35.046333 9.2139 6.7994 5.430 .0000 301.0000 -119.119033 35.046333 9.3553 6.9068 5.450 • Spectral response at 0.3, 1, 3 sec. .0000 301.0000 -119.085700 35.046333 9.4666 6.9888 5.470 .0000 301.0000 -119.052367 35.046333 9.6375 7.1221 5.4900 17.4121 100 17.3074 8.3918 1.7094 1.0000 301.0000 -119.019033 35.046333 9.7721 7.2250 5.5100 17.6918 8.6458 1.7203 1.0000 301.0000 -119.002367 35.046333 9.8200 7.2604 5.5200 17.7920 8.6879 1.7287 1.0000 301.0000 -118.985700 35.046333 9.8701 7.2979 5.5200 17.8972 8.7327 1.7376 1.0000 301.0000 -118.969033 35.046333 9.9507 7.3618 5.5400 18.0659 8.8099 1.7532 1.0000 301.0000 110 050267 25 046222 10 0205 7 4071 5 5500 1





Fault size (black line) scaling with magnitude



PERCEIVED SHAKING	Not felt	Weak	Light	Moderate	Strong	Very strong	Severe	Violent	Extreme
POTENTIAL DAMAGE	none	none	none	Very light	Light	Moderate	Moderate/Heavy	Heavy	Very Heavy
PEAK ACC.(%g)	<.17	.17-1.4	1.4-3.9	3.9-9.2	9.2-18	18-34	34-65	65-124	>124
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INSTRUMENTAL INTENSITY	- 1	11-111	IV	V	VI	VII	VIII	IX	X+



Processed: Mon Mar 1 17:16:41 2010

Automatic Global GMPE Selector



Daniel Garcia, USGS

A Global Earthquake Discrimination Scheme to Optimize Ground-Motion Prediction Equation Selection

by D. García, D. J. Wald, and M. G. Hearne

Abstract We present a new automatic earthquake discrimination procedure to determine in near-real time the tectonic regime and seismotectonic domain of an earthquake, its most likely source type, and the corresponding ground-motion prediction

equation (GMPE) class to be used in the U.S. ShakeMap system. This method makes use of scheme, seismotectonic information (plate bound alogs, and regional and local studies), and the s USGS National Earthquake Information Center in to give the best estimation of the setting and me the tectonic setting, additional criteria based on and regional seismicity may be applied. For sub the use of focal mechanism information and deta among outer-rise, upper-plate, interface, and i validated against a large database of recent histo to assess GMPE selection in Global ShakeMap (uses for this strategy, from real-time processing tectonic classification of sources from seismic (

Online Material: Tables and figures summi scheme and its performance.



Hayes' Slab1.0

What Are the Primary ShakeMap Uses?

Rapid, post-earthquake response, coordination, & situational awareness...





California Governor Schwarzenegger pointing to ShakeMap a his press conference following the M5.4 Chino Hills, Los Angeles, earthquake.

What Are the Primary ShakeMap Uses?

Mitigation thru earthquake scenarios (planning, response exercises, education) ...



What Are the Primary ShakeMap Uses?

Enhanced post-earthquake loss-assessment...


Earthquake Information Timeline



ShakeCast

What is ShakeCast?

- Open-source USGS software.
- Automatically retrieves ShakeMap & compares shaking levels with unique facility fragilities.
- Generates web pages & hierarchical lists & maps of likely impacted facilities (right).
- Sends notifications to specified personnel/responders.
- Raises post-earthquake situational awareness; represents key information in first min to hrs following an event.

manmin



* MMI level may extend beyond map boundary; some facilities may not appear on the map due to space restriction





ShakeCast Software: "primarily a database"



ShakeCast Cloud Workflow

Create an Amazon Cloud (AWS) Account, get approval, & load the ShakeCast Instance

Configure access/security settings

Input inventory, fragility, & notification databases (drag & drop)

Customize your monitoring regions, user notifications, products, & GUI

Bridge Fragility

- Bridge fragility method is based upon work originally published by Basöz and Mander.
- Method was implemented in FEMA's HAZUS-MH software.
- Uses data from National Bridge Inventory (NBI) as inputs:
 - Year built
 - Year improved or retrofit
 - Angle of skew
 - Bridge type
 - Number of spans
 - Maximum span length
 - Total bridge length
 - Deck width



L. Turner, Caltrans

Federal Highway (FHWA)/DOT National Bridge Inventory (NBI) → ShakeCast Fragility look-up tables

0										
0										
_	1 A	B	C	D	E	F	G	H		
1	external_facility_id	facility_type	facility_name	description	lat	lon	METRIC:PSA10:GREEN METR	IC:PSA10:YELLOW METRI	C:PSA10:ORANGE METR	IC:PSA10:RED
2	001001C	BRIDGE	001001C - BEAVER RIVER	1-span; 3; 02; 10 deg skew; 7.3 m Max Span Length; NBI Class 302; HAZUS Class HWB24; Built 1945;	38.26633	-112.63272	10	39.94	51.36	79.89
3	001002F	BRIDGE	001002F - BEAVER RIVER	1-span; 5; 04; 0 degskew; 7.6 m Max Span Length; NBI Class 504; HAZUS Class HWB3; Built 1985;	38.27233	-112.01350	10	115	138	195.5
	0010030	BRIDGE		1-span; 5; 10; 0 doe skew; 10.5 m Max Span Length; NBI Class 510; HAZUS Class HWB24; built 1925;	38,23233	-112.78919	10	40.25	127.74	105 13
6	0010040	BRIDGE	001005E - BEAVER RIVER	1-span, 5, 04, 0 deg skew, 0.1 m Max Span Length, NBI Class 119, MA203 Class HWB4, Built 1998,	38 25097	-112.33053	10	114.78	137.74	195.15
7	001005V	BRIDGE	001006V - DRY WASH	4-span; 3: 19: 0 deg skew; 1.8 m Max Span Length; NBI Class 319: HAZUS Class HWB3; Built 2005;	38.38472	-113.00977	10	99.67	137.04	211.79
8	001007F	BRIDGE	001007F - BEAVER RIVER	1-span; 5; 02; 6) deg skew; 20.1 m Max Span Length; NBI Class 502; HAZUS Class HWB4; Built 2004;	38.21806	-112.90167	10	81.32	97.58	138.24
9	001008V	BRIDGE	001008V - DRY WASH	4-span; 3; 19/0 deg skew; 1.8 m Max Span Length; NBI Class 319; HAZUS Class HWB14; Built 2005;	38.33833	-113.00972	10	99.67	137.04	211.79
10	001009E	BRIDGE	001009E - NORTH CREEK	2-span; 2, 19; 40 deg skew; 4 m Max Span Length; NBI Class 219; HAZUS Class HWB10; Built 1982;	38.29767	-112.64844	10	105.53	128.99	175.89
11	001010C	BRIDGE	001010C - BEAVER RIVER	span; 3; 02; 0 deg skew; 8.4 m Max Span Length; NBI Class 302; HAZUS Class HWB24; Built 1935;	38.27583	-112.60139	10	40.25	51.75	80.5
12	001011E	BRIDGE	001011E - NORTH CREEK	1-span; 1; 19; 60 deg skew; 6.7 m Max Span Length; NBI Class 119; HAZUS Class HWB3; Built 1985;	38.30628	-112.639	10	81.32	97.58	138.24
13	001012V	BRIDGE	001012V - NORTH CREEK	2-span; 3; 19; 30 deg skew; 3.7 m Max Span Length; NBI Class 319; HAZUS Class HWB24; Built 1985;	38.25458	-112.70144	10	37.46	48.16	74.91
14	001013V	BRIDGE	001013V - DRY WASH	4-span; 4; 19; 34 deg skew; 1.8 m Max Span Length; NBI Class 419; HAZUS Class HWB16; Built 2005;	38.30611	-113.01	10	104.6	127.85	174.34
15	001014V	BRIDGE	001014V - DRY WASH	4-span; 3; 19; 15 deg skew; 2 m Max Span Length; NBI Class 319; HAZUS Class HWB14; Built 2005;	38.31694	-113.00972	10	97.95	134.69	208.15
16	003001F	BRIDGE	003001F - MALAD RIVER	1-span; 5; 04; 0 deg skew; 14.9 m Max Span Length; NBI Class 504; HAZUS Class HWB3; Built 1930;	41.97614	-112.21631	10	115	138	195.5
17	003002F	BRIDGE	003002F - MALAD R VER	1-span; 5; 04; 0 deg skew; 14.9 m Max Span Length; NBI Class 504; HAZUS Class HWB4; Built 1991;	41.94397	-112.19711	10	115	138	195.5
18	0030030	BRIDGE								
20	0030040	BRIDGE	description							
20	0030080	BRIDGE								
22	003009V	BRIDGE	1-span: 3: 0	2: 10 deg skew: 7.3 m Max Span Length: NB	BI Clas	s 302:	: HAZUS Class	HWB24: Bi	uilt 1945:	
23	003010V	BRIDGE		-,,,		,	,		,	
24	003011F	BRIDGE	1-span: 5:0	4·0 deg skew: 7.6 m Max Span Length: NBL	Class	504.1	HA7HS Class F	4W/R3+ Ruilt	1985	
25	003012A	BRIDGE	1 Spuil, 5, 0	t, o deg skew, 7.0 m max span tengen, ron	Clubb	504,1	IA205 Class I	revos, build	. 1909,	
26	003013C	BRIDGE	1-cnan: 2.1	0. 0 deg skow: 18 3 m May Span Length: NB	I Clas	c 210	HATUS Class	H\A/B24+ Bi	il+ 1022	
27	003014F	BRIDGE	T-shaii, 2, T	o, o deg skew, 10.5 m wax span Length, No	n Clas	5 510,	, HALUS Class	HVVDZ4, D	unt 1925,	
28	003015D	BRIDGE	1 anony 1, 10; E dog allowy C 1 m May Snon Longth, NDI Class 110; UAZUS Class UN/DA, Duilt 1000							
29	003016D	BRIDGE	1-span; 1; 1:	9; 5 deg skew; 6.1 m iviax Span Length; ivBi	Class	113,1	HAZUS Class F	1VV 84; Built	1998;	
30	003017C	BRIDGE								
31	003018D	BRIDGE	003018D - WEST CANAL	1-span; 1; 07; 0 deg skew; 10.4 m Max Span Length; NBI Class 107; HAZUS Class HWB4; Built 1991;	41.81389	-112.15883	10	115	138	195.5
32	003019D	BRIDGE	003019D - MALAD RIVER	1-span; 1; 07; 0 deg skew; 12.2 m Max Span Length; NBI Class 107; HAZUS Class HWB3; Built 1958;	41.81428	-112.13797	10	115	138	195.5
33	003020F	BRIDGE	003020F - WEST CANAL	1-span; 5; 04; 0 deg skew; 14.3 m Max Span Length; NBI Class 504; HAZUS Class HWB3; Built 1960;	41.831/2	-112.12633	10	115	138	195.5
34	0030210	BRIDGE		1-span; 1; 01; 45 deg skew; 6.4 m Max Span Length; NBI Class 101; HAZOS Class HWB3; Built 1920;	41.50606	-112.1773	10	90.7	110.04	104.4
36	0030221	BRIDGE	003022F - MALAD RIVER	1-span, 3, 04, 0 deg skew, 11 m Max Span Length, NBI Class 304, HAZUS Class HWB3, Built 1950,	41.85738	-112.15850	10	40.25	51.75	80.5
37	003024C	BRIDGE	003024C - WEST CANAL	1-span; 3: 02: 0 deg skew: 9.4 m Max Span Length; NBI Class 302: HAZUS Class HWB24; Built 1948:	41.82847	-112.15544	10	40.25	51.75	80.5
38	003025D	BRIDGE	003025D - WEST CORINNE C	A 1-span; 1: 01: 45 deg skew: 8.5 m Max Span Length: NBI Class 101: HAZUS Class HWB3: Built 1945:	41.55658	-112.17814	10	96.7	116.04	164.4
39	003026F	BRIDGE	003026F - WEST CANAL	1-span; 5; 04; 0 deg skew; 10.4 m Max Span Length; NBI Class 504; HAZUS Class HWB3; Built 1945;	41.82472	-112.07828	10	115	138	195.5
40	003028C	BRIDGE	003028C - CORINNE CANAL	2-span; 3; 02; 15 deg skew; 3.7 m Max Span Length; NBI Class 302; HAZUS Class HWB24; Built 1940;	41.80731	-112.10825	10	39.56	50.86	79.12
41	003030D	BRIDGE	003030D - WEST CANAL	1-span; 1; 07; 29 deg skew; 6.4 m Max Span Length; NBI Class 107; HAZUS Class HWB4; Built 1993;	41.70919	-112.28639	10	107.55	129.06	182.83
42	003031F	BRIDGE	003031F - BEAR RIVER	4-span; 5; 02; 40 deg skew; 22.3 m Max Span Length; NBI Class 502; HAZUS Class HWB17; Built 1972;	41.63858	-112.11867	10	35.23	45.29	70.46
43	003033C	BRIDGE	003033C - CORINNE CANAL	1-span; 3; 02; 0 deg skew; 8.5 m Max Span Length; NBI Class 302; HAZUS Class HWB24; Built 1945;	41.65478	-112.14066	10	40.25	51.75	80.5
44	003034F	BRIDGE	003034F - MALAD RIVER	1-span; 5; 04; 0 deg skew; 9.1 m Max Span Length; NBI Class 504; HAZUS Class HWB3; Built 1978;	41.65539	-112.15997	10	115	138	195.5
45	003035V	BRIDGE	003035V - MALAD RIVER	1-span; 3; 19; 0 deg skew; 9.1 m Max Span Length; NBI Class 319; HAZUS Class HWB4; Built 2001;	41.65339	-112.16275	10	115	138	195.5
46	003037F	BRIDGE	003037F - MALAD RIVER	1-span; 5; 04; 0 deg skew; 14.6 m Max Span Length; NBI Class 504; HAZUS Class HWB3; Built 1969;	41.66872	-112.15556	10	115	138	195.5
47	003038E	BRIDGE	003038E - CORINNE CANAL	1-span; 1; 19; U deg skew; 6.1 m Max Span Length; NBI Class 119; HAZUS Class HWB3; Built 1967;	41.67/78	-112.14158	10	115	138	195.5
48	0030390	PRIDGE	003040C - MALAD RIVER	1-span; 5; 02; 0 deg skew; 7.9 m Max Span Length; NBI Class 302; HAZUS Class HWB24; Built 1945; 1-span; 2: 02: 0 deg skew; 11.6 m Max Span Length; NBI Class 202; HAZUS Class HWB24; Built 1945;	41.08322	-112.141/5	10	40.25	51./5	80.5
49	0030400	BRIDGE	003040C - IVIALAD KIVEK	1-span, S, VZ, V deg skew; 11.0 m ividx span Length; NBI Class 302; HAZUS Class HWB24; Built 1945; 3-span: 4: 09: 0 deg skew; 22.9 m May Span Length; NBI Class 400: UA7US Class UM/P15; Built 1945;	41.08328	-112.15501	10	40.25	51./5	6U.5 128 61
51	003042E	BRIDGE	003042E - MALAD RIVER	1-snan: 5: 04: 0 deg skew: 14.9 m Max Snan Length: NBI Class 504: HA7US Class HWB13; Built 1945;	41.69736	-112 16183	10	115	138	195.5
52	003043F	BRIDGE	003043F - CORINNE CANAL	1-span: 5: 04: 0 deg skew: 6.7 m Max Span Length: NBI Class 504: HAZUS Class HWB3: Built 1905;	41.70503	-112.14242	10	115	138	195.5
53	003044F	BRIDGE	003044F - MALAD RIVER	1-span; 5; 04; 0 deg skew; 15.2 m Max Span Length: NBI Class 504; HAZUS Class HWB3; Built 1965;	41.72658	-112.15078	10	115	138	195.5
54	0030455	RRIDGE	002045E - WEST CANAL	1 snan: 1: 10: 45 dag skow: 10.1 m Max Snan Longth: NBI Class 110: HA7US Class HWR2: Built 1099.	/1 7255	_112 10556	10	06.7	116.04	164.4
14.4	UT12_sc.csv / +) 4 1-



I-TEAM BRIEF



The Innovation Team (I-Team) at the Caltrans Division of Research and Innovation, in cooperation with its partners, develops proven, ready-to-deploy innovations in methods, materials, and technologies that enable Caltrans to provide the most effective management of public services, resources, and infrastructure.

DIVISION OF RESEARCH AND INNOVATION

A post-earthquake decision-making and rapid-response tool

After a major earthquake, one of Caltrans' most critical tasks is to assess the impact on the condition of all bridges and roadway corridors in the state highway system. Timely response ensures public safety, guides emergency vehicle traffic, and reestablishes critical lifeline routes. Without sufficient data, initial reconnaissance takes up precious time. The Caltrans I-Team adopted ShakeCast, a tool that uses data from an earthquake event to support rapid post-earthquake response.

READY TO DEPLOY

ShakeCast

ShakeCast is a Web-based application that automatically retrieves measured earthquake shaking data and analyzes the data in relation to individual bridge performance characteristics. By focusing inspection efforts on the most damage-susceptible infrastructure in the most severely shaken areas, ShakeCast has drastically reduced Caltrans' response time to assess potentially damaged structures after an earthquake.

NEW AND IMPROVED

- Retrieves measured shaking data within minutes after an earthquake.
- Compares shaking distribution with unique bridge vulnerabilities.
- Provides hierarchical lists and maps of bridges most likely impacted.
 Emails bridge and facility location and inspection priority information to
- responders within 15 minutes following events with a magnitude greater than 4.0.
- Automatically generates products for direct use in Google Earth®, ArcGIS®, and Excel®.
- Provides a suite of tools on ShakeCast website.



SEPTEMBER 2010 Updated: October 2010

Performance of the Caltrans ShakeCast System in the 2014 Napa M6.0 Earthquake

September 19, 2014

Prepared by:

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Gallman

Loren L. Turner, P.E. Division of Research, Innovation & System Information 5900 Folsom Blvd, MS-5, Sacramento, CA 95819 loren.turner@dot.ca.gov

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Caltrans Division of Research, Innovation and System Information

ShakeCast Import Spreadsheet



Example ShakeCast User Sectors, Users, Facility Types & Uses

	U.S. Nuclear Regulatory Commission (USNRC)	U.S. Nuclear Power Plants (NPP)	Awareness of regulatory shaking thresholds at domestic NPPs		
Critical Facilities	International Atomic Energy Agency (IAEA)	Global Nuclear Power Plants (NPP)	Awareness of shaking at NPPs for IAEA's External Event Notification System at International Seismic Safety Center, Vienna		
Critical Facilities	Veteran's Administration (VA)	VA Hospitals	Alerts sent to specific responsible personnel		
	California's Office of Statewide Health Planning and Development (OSHPD)	California's Healthcare infrastructure	Notification to engineering experts		
	California Department of Transportation (Caltrans)	20,000 overpasses & bridges statewide	Prioritize bridge inspection; Alert >300 engineers, inspectors, maintenance crews		
Transportation	Port of Long Beach (POLB)	Port infrastructure & utilities	Activate incident management for rapid inspections; work-around strategies for impacted infrastructure; ensure POLB remains open for business		
Lifelines/Utilities	Los Angeles Dept. of Power & Water (LADPW)	Over 5000 county facilities, including dams, water tanks, buildings, & survey monuments.	Used by the Earthquake Bridge Inspection Teams to prioritize inspections; >150 administrators, inspectors, engineers, & coordinators receive structure reports.		
	East Bay Metro. Utility District (EBMUD)	100's of dams, pipelines, control buildings, & facility structures			
Private/Business	Walmart	4,200 retail outlets,148 distri- bution centers, 50 corporate facilities; 1.6M associates	Situational awareness for emergency operations; "Taking care of our people, operations, communities"		
	Target	1700+ Locations	Rapid reporting of earthquake damage potential, prioritization of assessment and inspection		
Education	LA Unified School District (LAUSD)	1096 Schools/Office locations serving 740,000 students; 80,000 employees	Generate priority list for inspection; schools that can receive displaced students; clarify locations for Red Cross Shelters.		
	University of Southern California (USC)	Campus buildings			
Engineering	Degenkolb Engineering	Hospitals, varied engineered structures	Post earthquake inspection, priorities, as a customer service		
	ImageCat, Inc.	varied engineered portfolios	trigger in-house loss-estimation software as customer service		

PAGER

Prompt Assessment of Global Earthquakes for Response

















USGS ShakeMap Estimated Shaking Intensities

[Same Map Scales!]

Epicenter and Magnitude

[Same Map Scales!]



ShakeMap Atlas: ShakeMaps for >6,000 Earthquakes (1973-2012)





PAGER Empirical Fatality Model Ingredients



PAGER's Empirical Fatality Estimation Approach:



Jaiswal et al. (2009) & Jaiswal & Wald (2010)

Empirical Fatality Estimation Approach:

Fatality rate is parameterized with a two-parameter lognormal CDF:

$$F(I_i) = \phi\left(\frac{1}{\beta}\ln\left(\frac{I_i}{\theta}\right)\right)$$

Where I_i is intensity at level *i* and $\Theta \& \beta$ distribution parameters. The total number of fatalities for an earthquake can be estimated as:

Fatalities
$$E = \sum_{i} F(s_i) P(s_i)$$

For a given region/country, we use several historical earthquakes in order to derive parameters $\theta \& \beta$.

We solve for the two parameters which minimizes norm *e*:

$$e_{k} = \ln\left(\sqrt{\frac{1}{N}\sum_{j}\left(E_{j} - O_{j}\right)^{2}}\right) + \sqrt{\frac{1}{N}\sum_{j}\left[\ln\left(E_{j} / O_{j}\right)\right]^{2}}$$

PAGER Empirical National Methodology



Fatality rates as a function of intensity for selected countries

Economic Model Input Dataset:







- Earthquake, tsunami, volcanic eruption
- Storm
- Flood
- Extreme temperature (heat wave, forest fires)

Great natural catastrophes:

- Earthquake China
- Hurricane Ike
 Cyclone Nargis
- Winter damage China



3. Munich Re NatCAT Service 1980-2007 available through--



A world of information

PAGER: Semi-Empirical Model





Jaiswal and Wald (2008)

PAGER Structure Taxonomy ("PAGER-STR")

Label	Description	Detailed Classification (Based on ATC-13, HAZUS 1999, WHE 2003, EMS 1998 and newly added for PAGER Inventory database 2008)				
W	Wood	W1 (Wood with stucco, veneer), W2 (Heavy wood frame, >=5000 sf), W3 (Wood with metal strong wall) and W4 (log building)				
S	Steel	S1 (Steel moment frame of low, mid and high rise), S2 (Steel braced frame of low, mid and high rise), S3 (Steel light frame), S4 (Steel frame with concrete shear wall of low, mid and high rise), S5 (Steel frame with URM wall of low mid and high rise)				
С	Reinforced Concrete	C1 (Ductile RC moment frame of low, mid and high rise), C2 (RC shear-wall of low, mid and high rise), C3 (Nonductile RC frame with infill of low, mid and high rise), C4 (Nonductile RC frame without infill of low, mid and high rise), C5 (Steel reinforced concrete frame of low mid and high				
RM	Reinforced Masonry	R1 (Reinforced masonry bearing wall with flex rigid diaphragm of low, mid and high rise) • >100 Structure Types				
MH	Mobile Homes	Mobile homes • Composite of:				
М	Mud	M1 (Mud wall without wood), M2 (Mud wall) \bigcirc ATC-13 California				
A	Adobe	A1 (Adobe mud mortar with wood roof), A2 (A (Adobe wall with concrete bond beam), A5 (A O FEMA' 99 (HAZUS), U.S.				
RE	Rammed Earth	Rammed earth construction O EMS' 98, Euro-Med				
RS	Rubble (Field) Stone	RS1 (Rubble stone without mortar), RS2 (Rub stone with cement mortar), RS5 (Rubble stoneOEERI/WHE' 03, Global OOPAGER definitions, missing types				
DS	Dressed Stone, blocks	DS1 (Stone block with mud mortar), DS2 (Stor block with concrete bond beam)				
UFB	Unreinforced Fire Brick	UFB1 (Unreinforced brick with mud mortar without timber), UFB2 (Unreinforced brick with mud mortar and timber), UFB3 (Unreinforced brick with cement mortar and wood diaphragm), UFB4 (Unreinforced brick with cement mortar and concrete diaphragm)				
UCB	Unreinforced Concrete Block	Unreinforced concrete block construction				
MS	Massive Stone	Massive stone masonry construction				

Collapse Fragility Modeling



RC-T2: Nonductile gravity-load bearing RC regular frame with masonry infill walls (4 to 7 stories)

Population Distribution

Data/Expert Judgment Similar to HAZUS Principles

Time of day vs. occupancy type	Residential Occupancy	Non-residential Occupancy	Outside (Outdoors)	
Day (10 am-5 pm)	$\begin{array}{c} P_{i}*(0.4*F_{nwf}+0.01*F_{wf}*F_{ind}\\ +0.01*F_{wf}*F_{ser}+0.01*F_{wf}*\\ F_{agr})P_{i}*(0.75*F_{nwf}+0.20*F_{wf}*\\ F_{ind}+0.25*F_{wf}*F_{ser}+0.45*F_{wf}*\\ F_{agr})P_{i}*(0.999*F_{nwf}+0.84*F_{wf}*\\ F_{ind}+0.89*F_{wf}*F_{ser}+0.998*F_{wf}*\\ F_{agr})\end{array}$	$\begin{array}{l} P_{i}^{*}(0.89^{*}F_{wf}^{*}F_{ind}^{*}+0.89^{*}F_{wf}^{*}\\ F_{ser}^{}+0.34^{*}F_{wf}^{*}F_{agr}^{}+0.25^{*}F_{nwf}^{*}\\ F_{sch}^{})P_{i}^{*}(0.25^{*}F_{wf}^{*}F_{ind}^{}+0.25^{*}F_{wf}^{}\\ ^{*}F_{ser}^{}+0.01^{*}F_{wf}^{*}F_{agr}^{})P_{i}^{*}(0.15^{*}\\ F_{wf}^{*}F_{ind}^{}+0.10^{*}F_{wf}^{*}F_{ser}^{}+0.001^{*}\\ F_{wf}^{*}F_{agr}^{})\end{array}$	$\begin{array}{c} P_{i}^{*}(0.35^{*}\ F_{nwf}^{}+0.10^{*}\ F_{wf}^{}*\ F_{ind}^{}\\ +0.10^{*}\ F_{wf}^{}*\ F_{ser}^{}+0.65^{*}\ F_{wf}^{}*\\ F_{agr}^{})P_{i}^{*}(0.25^{*}\ F_{nwf}^{}+0.55^{*}\ F_{wf}^{}*\\ F_{ind}^{}+0.50^{*}\ F_{wf}^{}*\ F_{ser}^{}+0.54^{*}\ F_{wf}^{}*\\ F_{agr}^{})P_{i}^{*}(0.001^{*}\ F_{nwf}^{}+0.01^{*}\ F_{wf}^{}*\\ F_{ind}^{}+0.01^{*}\ F_{wf}^{}*\ F_{ser}^{}+0.001^{*}\ F_{wf}^{}*\\ F_{agr}^{})\end{array}$	
Transit (5 am-10 am & 5 pm- 10 pm)	$\begin{array}{c} P_{i} * (0.4*F_{nwf} + 0.01*F_{wf}^{*} \\ + 0.01*F_{wf} * F_{ser} + 0.01*F_{wf}^{*} \\ F_{agr})P_{i} * (0.75*F_{nwf} + 0.20*F_{wf}^{*} \\ F_{ind} + 0.25*F_{wf} * F_{ser} + 0.45*F_{wf}^{*} \\ F_{agr})P_{i} * (0.999*F_{nwf} + 0.84*F_{wf}^{*} \\ F_{ind} + 0.89*F_{wf} * F_{ser} + 0.998*F_{w} \\ F_{agr}) \end{array} + \begin{array}{c} \end{array}$	$F_{wf} * F_{ind} + 0.01 * F_{wf} *$ $+0.20 * F_{wf} * F_{ind}$ $F_{wf} * F_{ind}$		
Night (10 pm- 5 am)	$\frac{P_{i} * (0.4* F_{nwf} + 0.01* F_{wf} * F_{ind} + 0.01* F_{wf} * F_{ind} + 0.01* F_{wf} * F_{ser} + 0.01* F_{wf} * F_{agr})P_{i} * (0.75* F_{nwf} + 0.20* F_{wf} * F_{ind} + 0.25* F_{wf} * F_{ser} + 0.45* F_{wf} * F_{agr})P_{i} * (0.999* F_{nwf} + 0.84* F_{wf} * F_{ind} + 0.89* F_{wf} * F_{ser} + 0.998* F_{wf} * F_{agr})$			

Fatality Rates



Countries with Sufficient Earthquake Fatality Data





Global Inventory & Coverage





PAGER Regionalization Scheme (V2.0, Dec. 2010)





Kathmandu, Nepal, M8.1

General distribution of building types in the Kathmandu Valley (Dixit and Shrestha, 2005).



A: Adobe block

UFB: Unreinforced fired brick masonry walls with mud, lime, or cement mortar and timber joists used to support floor or roof (**UFB1** mud mortar with no timber joists)

DS: Dressed stone masonry walls (DS3 concrete mortar with timber floors and roof)

RS: Rubble stone masonry walls

W: Wood construction

C: Reinforced concrete frame construction (C1 engineered, C3 non-engineered)

Manan

UNK: Unknown construction



Kathmandu, Nepal, M8.1



Figure 7. A typical adobe (A) building in Jantanagar, Nepal (Photo Courtesy: Auroville Earth Institute, http://www.earth-auroville.com/ nepal_june_2008_en.php).

Figure 8. Example of an unreinforced fired brick (**UFB**) masonry building in Nepal (Photo Courtesy: NSET, Nepal).



Kathmandu, Nepal, M8.1



Science for a changing w	Svorld	- And the state of the second s		USGS Home Contact USGS Search USGS	
Earthquake Haz	zards Program	Home About Us	Contact Us	Search	
EARTHQUAKES	HAZARDS LEA	RN PREPARE	MONITORING	RESEARCH	
PAGER Home Archives Background onePAGER Information Team Members Data, Products, and References Data, Products, and References Data, Products, and Common Building Types FAQ Disclaimer Contact Us	PAGER - Common Algeria Single-family reinforced conc This privately owned housing cons widespread throughout northern Alg Generally, these buildings are one parking or for commercial purposes frames with masony infill walls ma provided in the residential part of the infill walls at the ground floor level, t during earthquakes. These building the 1981 Algerian seismic code. Ho construction and most of the buil provisions and historically have bee the May 21, 2003 Boumerdes eartho	Building Types rete frame houses titutes about 60 to 70% of the housing stor geria, the region of the country's highest sei to three stories high. The ground floor is . The structural system consists of reinforced de out of hollowper floors). Due to the limited a hese building upper floors. Due to the limited a hese buildings are characterized by soft-story is have most often been built after the develo lowever, the seismic code is not enforced if dings have been built without seismic strer in severely affected in Algerian earthquakes, juak.	k and is used for concrete behavior pment of behavior ghrening gincluding Izzali		
	Stone masonry apartment but This is a typical residential const constituting 40-50% of the total urbo the 1950s by French contractors, is four to six stories high. The slabs	ilding ruction type found in most Algerian urban un housing stock. This construction, built most no longer practiced. Buildings of this type are re wooden structures or shallow arches supp	centers, ly before typically orted by		

steel beams (jack arch system). Stone masonry walls, usually 400-600 mm thick, have adequate gravity load-bearing capacity; however, their lateral load resistance is very low As a result, these buildings are considered to be highly vulnerable to seismic effects.

Reference: EERI and IAEE\'s World Housing Encyclopedia (Report #75) - Mohammed Farsi, Farah Lazzali, Yamina Ait-M

Marnanew

Dixit, NSET Nepal).

Figu (**DS**

Nep



lonorced with

masonry infill (C3) construction (Photo Courtesy: NSET Nepal).



Analytical Approach



Yet more parameters are required! (many structural characteristics)






Earthquake Impact Scale

D. J. Wald¹; K. S. Jaiswal, A.M.ASCE²; K. D. Marano³; and D. Bausch⁴

Abstract: With the advent of the USGS prompt assessment of global earthquakes for response (PAGER) system, which rapidly assesses earthquake impacts, U.S. and international earthquake responders are reconsidering their automatic alert and activation levels and response procedures. To help facilitate rapid and appropriate earthquake response, an Earthquake Impact Scale (EIS) is proposed on the basis of two complementary criteria. On the basis of the estimated cost of damage, one is most suitable for domestic events; the other, on the basis of estimated ranges of fatalities, is generally more appropriate for global events, particularly in developing countries. Simple thresholds, derived from the systematic analysis of past earthquake impact and associated response levels, are quite effective in communicating predicted impact and response needed after an event through alerts of green (little or no impact), yellow (regional impact and response), orange (national-scale impact and response), and red (international response). Corresponding fatality thresholds for yellow, orange, and red alert levels are 1, 100, and 1,000, respectively. For damage impact, yellow, orange, and red thresholds are triggered by estimated losses reaching \$1M, \$100M, and \$1B, respectively. The rationale for a dual approach to earthquake alerting stems from the recognition that relatively high fatalities, injuries, and homelessness predominate in countries in which local building practices typically lend themselves to high collapse and casualty rates, and

these impacts lend to prioritization for international response. In contrast, fina response in regions or countries in which prevalent earthquake resistant construct fatalities. Any newly devised alert, whether economic- or casualty-based, shou procedures. Useful alerts should also be both specific (although allowably unce both simple and intuitive color-coded alerting criteria; yet the necessary uncer the alert to be over- or underestimated are preserved. The essence of the propose is now available in the immediate aftermath of significant earthquakes world EIS, PAGER's rapid loss estimates can adequately recommend alert levels and tainties; demanding or awaiting observations or loss estimates with a high level **NH.1527-6996.0000040.** © 2011 American Society of Civil Engineers.



CE Database subject headings: Earthquakes; Hazards; Emergency services.

Author keywords: PAGER; Impact scale; Earthquake.

Introduction

Neither earthquake magnitude nor macroseismic intensity provides sufficient information to judge the overall impact of an earthquake. Whereas higher magnitude earthquakes have greater energy release vulnerability of the built environment, and the resilience of the communities affected. Whereas these factors can now, in part, be rapidly assessed following significant earthquake disasters, communicating the impact is still hampered by the lack of an appropriate lexicon.



[Wald et al (2011) Natural Hazards Review]

M7.8 Nepal Mainshock



Orange **≥USGS** Earthquake USMD USAID Shaking Alert **M 7.3. NEPAL** ANSSIMM PAGER Origin Time: Tue 2015-05-12 07:05:19 UTC (12:50:19 local) Version 3 Location: 27.84^oN 86.08^oE Depth: 15 km Created: 2 hours, 5 minutes after earthquake Orange alert level for shaking-related fatalities. Significant casualties are likely and the disaster Estimated Fatalities Estimated Economic Losses is potentially widespread. Past events with this alert level have required a regional or national level response. Yellow alert level for economic losses. Some damage is possible. Estimated economic losses are 0-1% GDP of Nepal. 10,000 10,000 Estimated Pop tion Exposed to Earthquake Shaking ESTIMATED POPULATIO EXPOSUBE (k = x1000) . .* 26k* 95,415k* 60.510k 3.886k 304k 67k 0 0 ESTIMATED MODIFIED MERCALLI INTENSITY VIII 11-111 IV V VI VII IX X+ PERCEIVED SHAKING Not felt Weak Light Moderate Strong Very Strong Severe Violent Extreme Resistant Structure none none none V. Light l iaht Moderate Moderate/He Heavy V. Heavy none Light Moderate Moderate/Heav V. Heavy none *Estimated exposu the map area. ~\$60M ~160 Populatio population per ~1 sq. km from Landscan Stru Öve n resides 5000 merable to in str 84 86°E 88°E earthquake shaking, though some resistant structures exist. The predominant vulnerable building types are unreinforced brick with mud and unknown/miscellaneous types construction Historical Earthquakes (with MMI levels): Date Max Shaking Dist. Mag. (UTC) (km) MMI(#) Deaths 29°N 1998-09-03 77 5.6 VII(21 1974-03-24 17 5.7 VIII/509 1988-08-20 131 6.8 VIII(12) Recent earthquakes in this area have caused secondary hazards such as landslides and liquefaction that might have contributed to losses Selected City Exposure MMI Citv Population VI Zhan < 1 VI Kodari 2 VI Bhaktapur < 1 VI Kathmandu 1,442 VI Zuobude < 1 VI Camqyai < 1 1,600 V Patna IV Gorakhpur 674 IV Dhankuta 22 IV Pokhara 2001 IV Gangtok 31k AGER content is automatically generated, and only considers losses due to structural damag

EndEan content is automatically generated, and only considers losses due to structural dama Limitations of input data, shaking estimates, and loss models may add uncertainty. http://earthquake.usgs.gov/pager bold cities appear on map (k = x1000) Event ID: us20002ejl

M7.3 Nepal Aftershock







Modified from J. Daniels, CatDat



M8.1 OFDA SCENARIO (DONE IN 2013)

M7.8 Nepal Earthquake



http://earthquake.usgs.gov/pager

Event ID: us20002926

USGS PAGER System

(Prompt Assessment of Global Earthquakes for Response)



Λ

177

25

50

38

13

18

238k

282k

877

242

215k



Q

http://earthquake.usgs.gov/pager



PAGER ALERTS (late 2010-2013)

PAGER (Prompt Assessment of Global Earthquakes for Response)



PAGER Prompt Assessment of Global Earthquakes for Response









USGS PAGER System

(Prompt Assessment of Global Earthquakes for Response)

COSTA RICA EARTHQUAKE

COSTA RICA QUAKE





PAGER

Prompt Assessment of Global Earthquakes for Response









Aug 12, 2012, M6.2 China

Aug 11, 2012, M6.4 Iran



No fatalities, some injuries & damage



Reported Losses

300 fatalities, extensive damage



Overall, the population in this region resides in structures that are highly vulnerable to earthquake shaking, though some resistant structures exist. The predominant vulnerable building types are adobe and unreinforced brick masonry with timber floor construction.

Historical Earthquakes (with MMI levels):

Date	Dist.	Mag.	Max	Shaking	
(UTC)	(km)		MMI(#)	Deaths	
2002-06-22	357	6.5	VIII(4k)	227	
1997-02-28	103	6.1	VIII(7k)	1100	
1990-06-20	251	7.4	IX(83k)	45000	

Recent earthquakes in this area have caused secondary hazards such as landslides that might have contributed to losses.

Selected City Exposure

from Ge	oNames.org		
MMI	City	Population	
VII	Ahar	94k	
V	Tabriz	1,425k	
IV	Ardabil	411k	
IV	Mincivan	6k	
IV	Hashtrud	17k	
IV	Marand	124k	
IV	Orumiyeh	577k	
IV	Rasht	595k	
IV	Zanjan	357k	
III	Yerevan	1,093k	
III	Erbil	933k	
bold cities appear on map (k = x			

Event ID: us201208110023

Event ID: us201208121047

<1

114

<1

http://earthquake.usgs.gov/pager





Magnitude 6.0 2014 South Napa, CA

Magnitude 5.8 2011 Mineral, VA



1 Fatality (Sept 5th) >\$450M Damage **Reported Losses**



PAGER content is automatically generated, and only considers losses due to structural damage. Limitations of input data, shaking estimates, and loss models may add uncertainty. http://earthquake.usgs.gov/pager

Structures Overall, the population in this region resides

in structures that are highly resistant to earthquake shaking, though some vulnerable structures exist

Historical Earthquakes (with MMI levels):

Date	Dist.	Mag.	Max	Shaking		
(UTC)	(km)	-	MMI(#)	Deaths		
1983-05-02	284	5.7	VIII(1k)	0		
1980-01-24	76	5.8	VII(31k)	1		
1989-10-18	132	6.9	IX(3k)	62		
Recent earthquakes in this area have caused secondary hazards such as landslides and liquefaction that might have contributed to losses						

Selected City Exposure

from G	eoNames.org	
MMI	City	Population
VIII	Napa	77
VII	Yountville	3
VII	American Canyon	19
VI	El Verano	4
VI	Sonoma	11
VI	Temelec	1
IV	Oakland	391
IV	San Francisco	805
Ш	Sacramento	466
Ш	Fremont	214
Ш	Stockton	292
hold c	ities annear on man	(k - x100)

Event ID: nc72282711



ders losses due to structural dar

25

http://earthquake.usgs.gov/pager

PAGER content is automatically generated, and only cons

Limitations of input data, shaking estimates, and loss models may add uncertainty

Structures:

No Fatalities ~\$200M Damage

Overall, the population in this region resides in structures that are resistant to earthquake shaking, though some vulnerable structures exist

Historical Earthquakes (with MMI levels):

There were no earthquakes with significant population exposure to shaking within a 400 km radius of this event.

Selected City Exposure

MM	l City	Population
VII	Louisa	2k
VI	Gordonsville	2k
VI	Newington	21k
VI	Orange	4k
VI	Weber City	1k
VI	Lake Monticello	10k
V	Virginia Beach	425k
v	Washington	552k
IV	Richmond	191k
IV	Baltimore	611k
IV	Annapolis	36k
hold a	rities annear on man	(k - x1000)

Event ID: us082311a

twitter

SOLPARTMENER SOLEAND SECURE

FEMA

Craig Fugate ADMINISTRATOR

FEMA's mission is to support our citizens and first responders to ensure that as a nation we work together to build, sustain, and improve our capability to prepare for, protect against, respond to, recover from, and mitigate all hazards.

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@jarvisdeberrytp subtropical refers to a system that has characteristics of both tropical and extratropical cyclones. www.hurricanes.gov

7 minutes ago via Twitter for BlackBerry® in reply to jarvisdeberrytp

Subtropical Depression strengthens into Subtropical Storm #Otto www.hurricanes.gov

about 1 hour ago via web

#USGS #PAGER - Prompt Assessment of Global #Earthquakes for Response: provides fatality & economic loss estimates http://goo.gl/kg5Q



From: "Bausch, Douglas" <<u>Douglas.Bausch@fema.dhs.gov</u>> Date: Sep 30, 2014 3:48 PM Subject: FW: M4.1 Earthquake - Kansas / **Green PAGER issued** / Rural area

FYI. How NWC uses PAGER:

From: FEMA-NWC Sent: Tuesday, September 30, 2014 9:32 AM To: Armed Forces Health Surveillance Center ; Army Domestic; Casey, Wanda; EOC DOC; Daruvalla, Sampson; Dept of Labor; DOE; Don Boyce; DSPMO; Dubois, Vincent; EnergyResponseCenter@hq.doe.gov; FEMA-Recovery-Geo; FEMA TOP LEVEL MANAGERS; FEMA-MOTF; FEMA-NCP-CRC-WATCH; Gunn, Abraham; HHS; HQ-FEMA-OEA-Senior Staff; Ives, Robert; Jackson, Liz; jfhq.ncrcc@tsa.dhs.gov; Jones, Julius; Judson, Paul; Matia, Matthew; Vineyard, Micheal; Monchek, Rafaela; Moncrief, Jane; NOC.FEMA; NOC.SWO.Restricted; FEMA-nrccps-ocia; Osborne, Andrew; Peerbolte, Stacy; Pendergrass, Michael M; Pentagon J3; Pirrone, Joel; Rodriguez, Jose I; RR-FCO; Sabata, Andrew; Shoemate, Justin; Singleton Sr, Jacques; FAA Significant Incident Response Group; Soucie, Eric; Stewart, James M (LMD); Sullivan, Robert; Tribble, Ahsha; Zohn, Ashley; Behnke, Matthew; Burkett, Ronald (OGA); Customs and Border Patrol (CBP); Villoch, Deborah; Jacques, Richard; DHS – Office of Health Affairs (DHS-OHA); DOJ/ATF (ESF 13); Erickson, Somer; Hall, Carol (OGA); Hylton, Roberto; FEMA-IGA; Kahley, Matthew (OGA); Kimzey, Samuel; Kimzey, Samuel (OGA); Kooper, Ronald LCDR; Hatley, Thomas (OGA); MacIntyre, Anthony (OGA); Macintyre, Anthony; **NOAA**-LNO; FEMA-PSR; Special Advisor for National Tribal Affairs; Tamillow, Michael; Sholas, Mac (OGA); Irwin, William (OGA); **USNORTHCOM** (for FEMA Logistics) ; Valcourt, Kenneth (OGA); White, Gregory (OGA); Albright, Thomas; Amparo, Alex; Anderson, Lars; Apodaca, Michael; Asst Secretary for DOE; Balint, Thomas; Biasco, Lon; Blanchard-Mbangah, Shauna M; Breslin, Thomas; Bresnahan, Michael; Brewster, Jared; Buras, Ryan; Burgess, Steven; Camp, Gwen; Campbell, Pauline; Carleton, John; Carlyle, Robert; Coen Jr, Michael; Dorko, Jeffrey; Dozor, Joshua; Dunn-Alexander, Roslyn; ESF-06-MASS-CARE; Eswood, Louis; FEMA-LRC-Chief; FEMA-NWC-NCR-Watch; FEMA-R8-RRCC-DIRECTOR; FEMA-Recovery-Reports; Fields, Kathy; Fox, Kathleen; Fugate, Craig; Gammon, Carla; Geiger, Paul; George, Michael S; Gillis, Carmeyia; Gonzalez, Waddy; Gorman, Chad; Gray, Patricia; Green, Matthew; Grimm, Michael; Gruber, Corey; Hart, Patrick; HQ-OEA **Directors**: Rabin, John: Jones, Berl: Jones, Julius M. Jr: Juskie, John: Kaufman, David: Keldsen, Donald: Kieserman, Brad: Kish, James: Kittrie, Zachary: Koziol, Lauralee: Lapinski, Michael: Lewis, Leviticus: Liggett,

SAMPLE PAGER ALERT RECIPIENTS



Example PAGER users: Inter-American Development Bank

Example of PAGER - USGS Report



people exposed to a given shacking intensity in every point.



Event Intensity and Exposure definitions The Event has to register a VII (or higher Modified Mercalli Intensity Scale - MMI), country population inside the General Co

Tet Madified

Earthquake Coverage: A hypothetical example

The Coverage Index (CI) calculation:

CI = (Total Affected Population – MiAP) *100 (MAP - MiAP)

Disaster Contingency Loans

Total Affected Population: 322.000

■MAP (5% of Country Population) = 5%*[10.000.000] = 500.000 ■*MiAP* (2% of Country Population) = 2%*[10.000.000] = 200.000

> (322.000 - 200.000) * 100 CI == 41% (500.000 - 200.000)

The Contingent Loan provides coverage for up to US\$100M. Therefore, an event with a CI of 68% would be eligible for a pay out of up to 41US\$M.

Mercalli Intensity	Perceived Shaking		
X	Extreme		,
IX	Violent	Heavy	V. Heavy
VIII	Severe	Moderate/Heavy	Heavy
VII	Very Strong	Moderate	Moderate/Heavy
VI	Strong	Light	Moderate
V	Moderate	V. Light	Light
IV	Light	None	None
II-III	Weak	None	None
I	Not Felt	None	None



Courtesy of J. Martinez, IDB

Weather EARTHQUAKE INFORMATION

EARTHQUAKE

MAY 12, 2015 07:05 UTC

Magnitude: 7.3

Depth: 18.5 KM

Region: 22KM SE OF ZHAM, CHINA

Pedram Javaheri ^(a)JavaheriCNN

COMBRK STAY WITH CNN FOR MORE ON THIS & THE LATEST INTERNATIONAL NEWS







USGS

USGS PAGER System (Prompt Assessment of Global Earthquakes for Response)



Wenchuan, China Mw 7.9. 2008 87,000 Fatalities (~20,000 killed by landslides)





PAGER content is automatically generated, and only considers losses due to structural damage Limitations of input data, shaking estimates, and loss models may add uncertainty

http://earthquake.usgs.gov/page

Neijiang Chongqing

IV

Event ID: us200805120628

3,967







Landslides & Liquefaction: ShakeCast Implementation

Requires:

- 1. USGS provide & distributed landslide & liquefaction likelihoods in ShakeMap-like grid (*geogrd.xml*).
- 2. ShakeCast retrieves geogrd.xml to provide users with site-specific likelihoods in categories for facility evaluation.



Requires:

- User has higher resolution/quality geotechnical information, e.g., susceptibility maps (separate landslide & liquefaction maps).
- Look up tables for peak motion → likelihood levels (low, medium, high, very high).



Map Version 1 Processed Thu Nov 29, 2012 05:20:46 PM MST

PEAK ACC.(%g)	<0.05	0.3	2.8	6.2	12	22	40	75	>139
INSTRUMENTAL INTENSITY	- 1	11-111	IV	V	VI	VII	VIII	IX	X+

Scale based upon Worden et al. (2011)

Candidate Explanatory Variables (Logistic Regression)

Landsliding



Triggering Input ShakeMap (PGA)

PGA



[A. Nowicki et al. (2014)]

Liquefaction

Soil Strength (Vs30)



Susceptibility "CTI or Wetness Index"



Triggering Input (PGA)



[J. Zhu et al. (2014)]

Nepal Mainshock & Aftershock Modeled Landslide Density



Sean Gallen (Univ. Mich & ETH Zurich)



ShakeCast

PAGER (Prompt Assessment of Global Earthquakes for Response)



ShakeCast

Kuo-wan Lin Daniel Slosky Vikki Appel PAGER (Prompt Assessment of Global Earthquakes for Response)

Kishor Jaiswal Mike Hearne Kristin Marano

"Did You Feel It?"

ShakeMap

Vince Quitoriano

Bruce Worden

Recent Collaborators & students

Nico Luco, USGS Jing Zhu, Tufts Emily So, Cambridge Univ Daniel Garcia, USGS Trevor Allen, USGS/GA/GSC

EERI/WHE Global Earthquake Model Douglas Bausch, FEMA Kendra Johnson, CSM Keith Porter, CU Boulder Eric Thompson, SDSU Anna Nowicki, Indiana Univ Keith Knudsen, USGS Russell Mah, CSM



Acknowledgments
ShakeCast

Landslide & Liquefaction Cloud Services National Databases (NBI, NID, HSIP) Stations@facility; Owner/CSN//QuakeCatcher, etc. **PAGER** (Prompt Assessment of Global Earthquakes for Response)

Atlas 2.0 Recalibration (China) Semi-emp; Analytic Models Sub-country inventories Non-shaking Losses Use cases Alert accuracy evaluation

"Did You Feel It?"

Responsive/Mobile Web Animation & Annual Maps Intensity Prediction Equations PSHA testing

ShakeMap

Scenario enhancements & standardization
Spatial Variability (esp. scenarios)
Site amplification improvements (empirical, Vs30, numerical)
3D simulations
<u>EEW cost/benefit</u> (warning time probabilities)

Work in progress...



ShakeCast

PAGER (Prompt Assessment of Global Earthquakes for Response)

Thank You!

"Did You Feel It?"

ShakeMap



